

Initiation of Dynamic Ruptures in Numerical Simulations

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- **introduction**
- critical parameters of the initiation zone (IZ) and their estimates
- effects of shape/aspect ratio on the IZ
- verification
- influence of material parameters of the IZ
- optimal parameters of the IZ
- summary

introduction

artificial procedures are used
to initiate dynamic ruptures
under linear slip-weakening friction law

the artificial initiation may have significant impact
on the resulting dynamic rupture propagation

therefore,

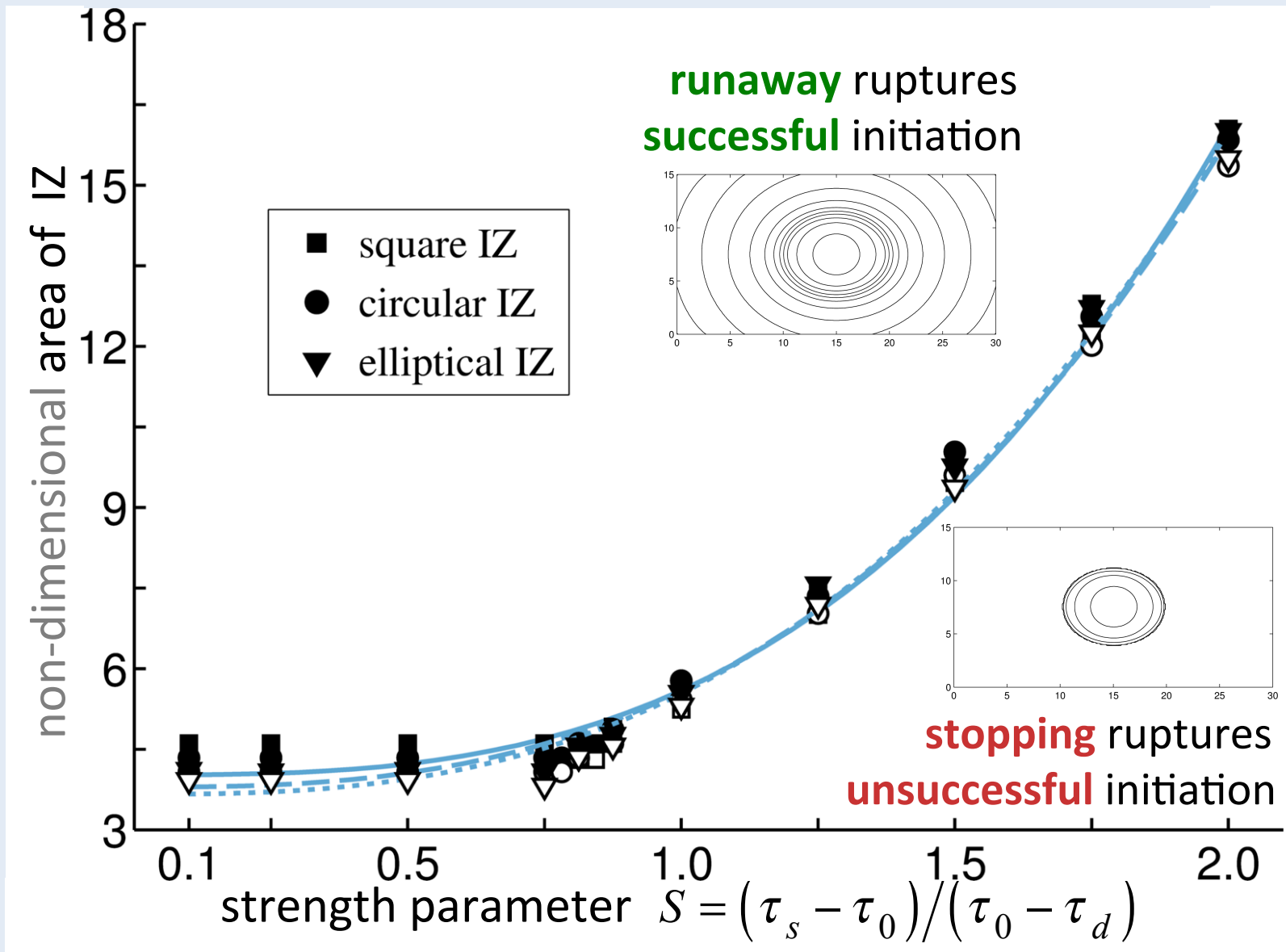
**it is desirable to understand and then minimize
side effects of the initiation**

here we discuss initiation

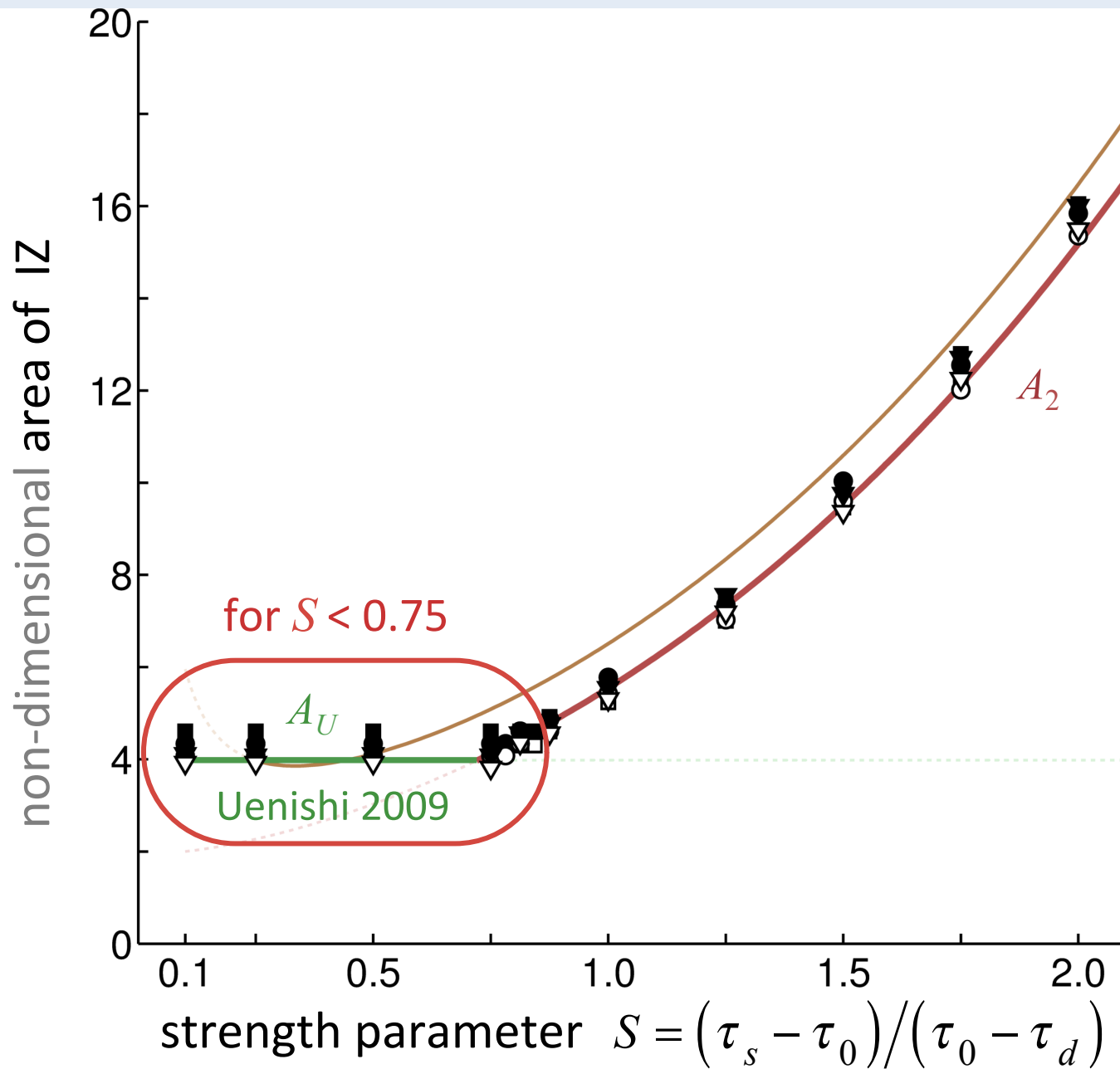
using an overstressed asperity,

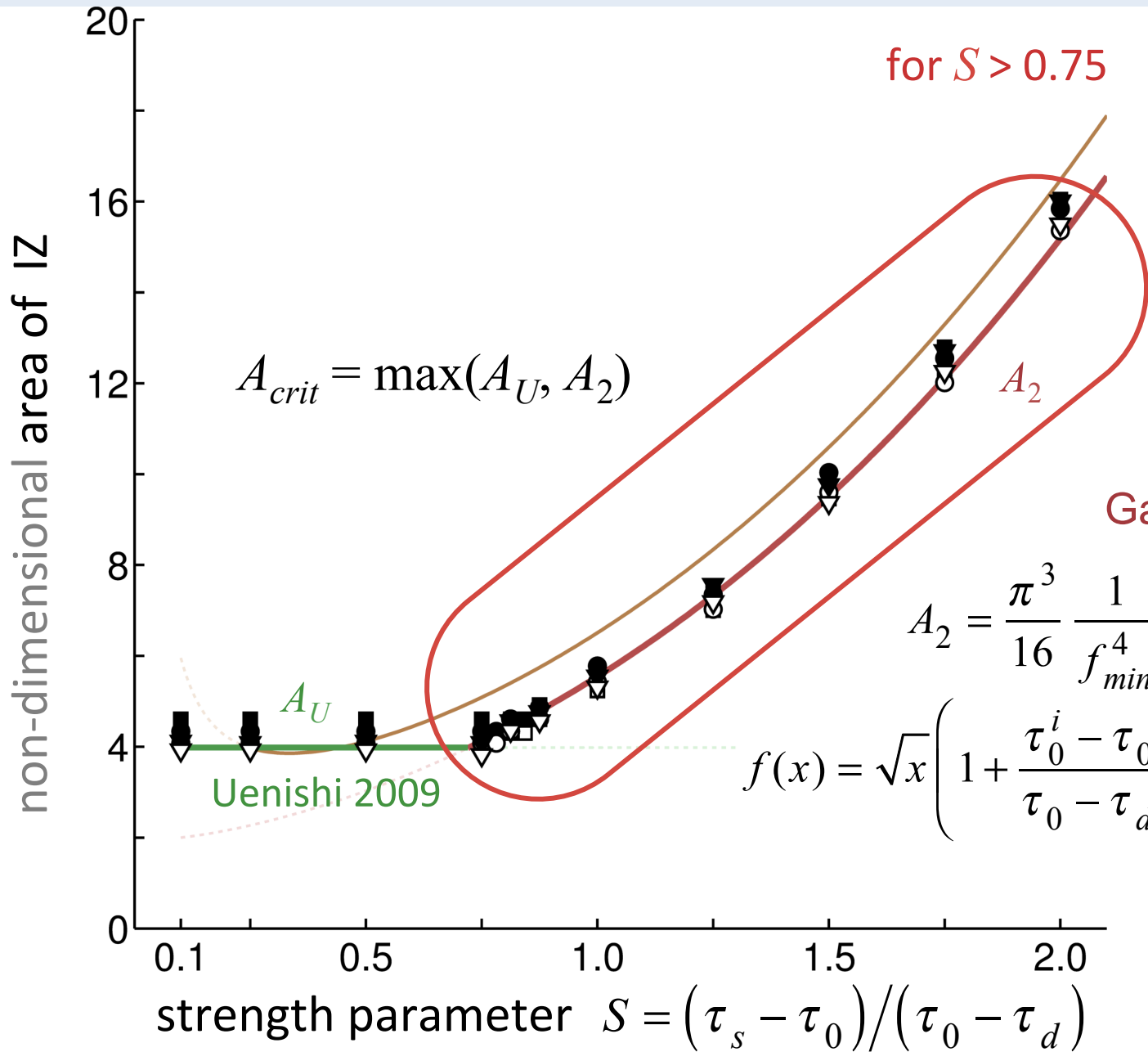
i.e., region with initial traction higher than static traction

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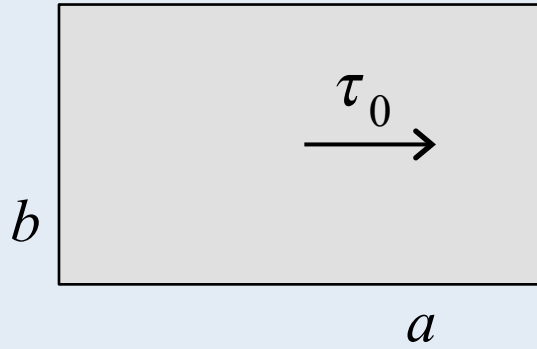
the initiation is controlled by the area of the initiation zone
(not by the half-length or shape)



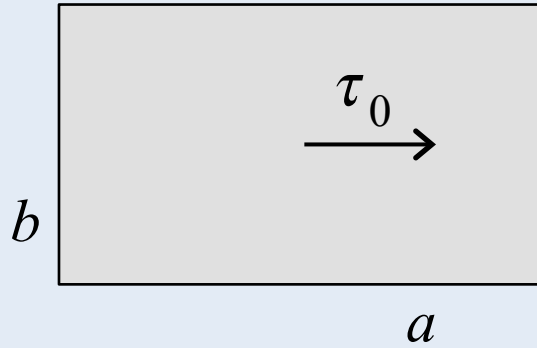


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effects of shape/aspect ratio on the IZ



effects of shape/aspect ratio on the IZ



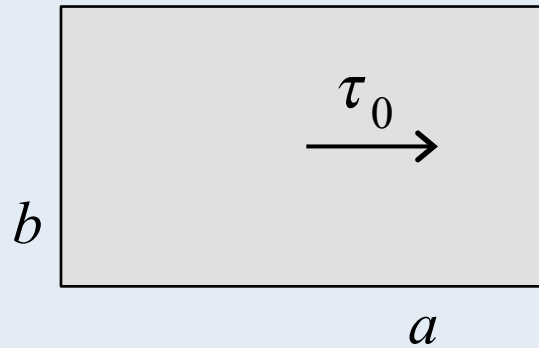
transition
from 3D

(init. controlled by area)

to 2D

(init. controlled by length)

effects of shape/aspect ratio on the IZ

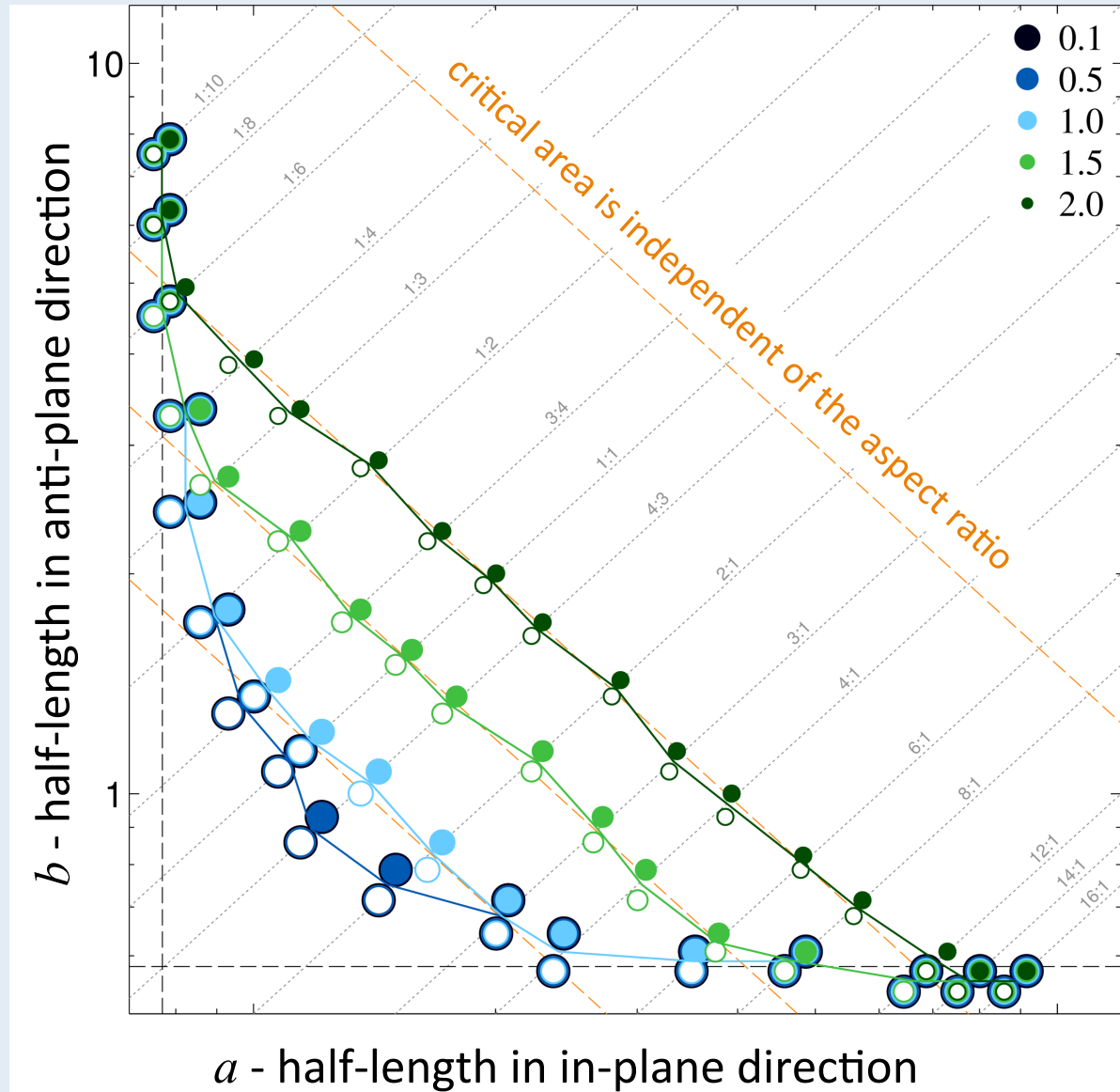


transition
from 3D

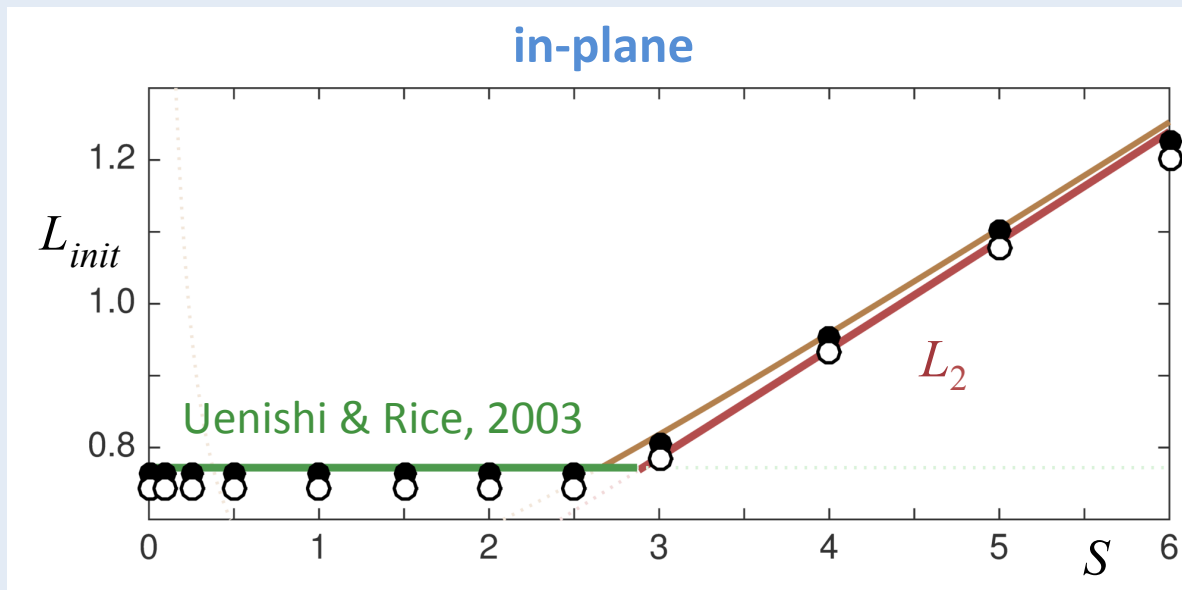
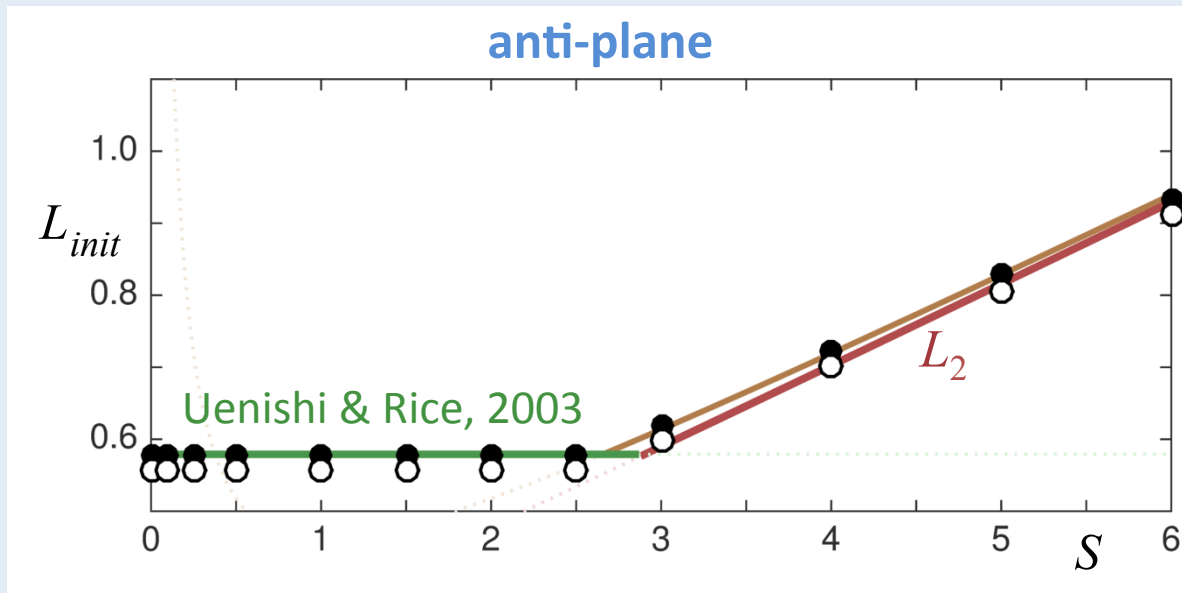
(init. controlled by area)

to 2D

(init. controlled by length)



effects of shape/aspect ratio on the IZ



outline

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to demonstrate that

our results and conclusions are not biased

by the choice of the numerical method,

we verify our results using

- **FESD**

2nd order finite-element method

Galis et al. (2008, 2010); Moczo et al. (2014)

- **SeisSol**

ADER-DG: arbitrary high-order derivative – discontinuous Galerkin method

Käser and Dumbser (2006), De la Puente et al. (2009), Pelties et al. (2012)

- **SORD**

2nd-order support operator method

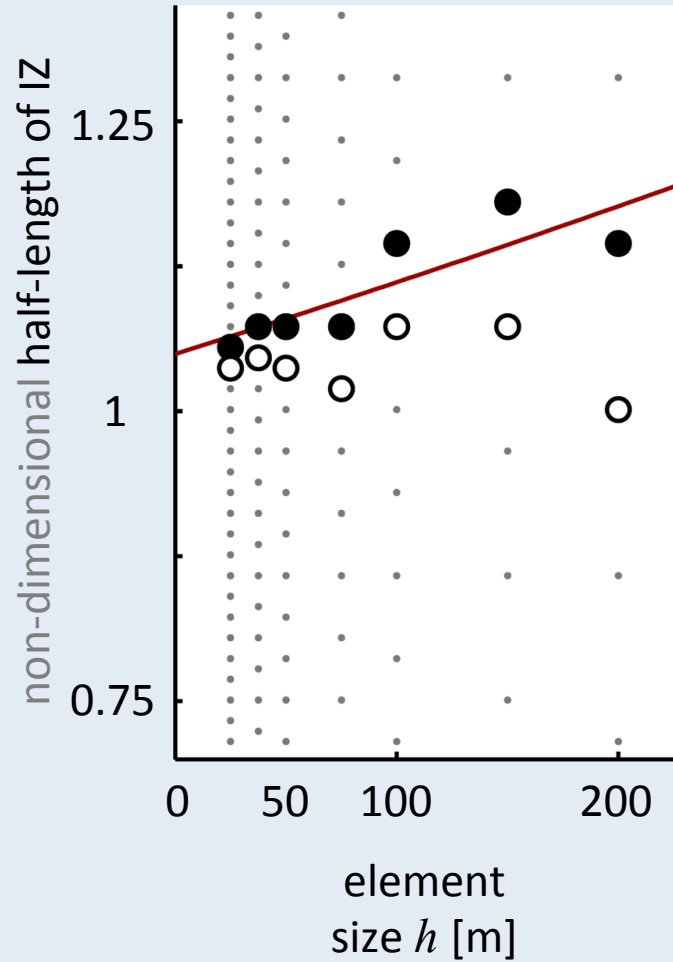
Ely et al. (2008, 2009)

- **WaveQLab3D**

6th-order summation-by-parts finite-difference method

Duru and Dunham (2015)

FEM



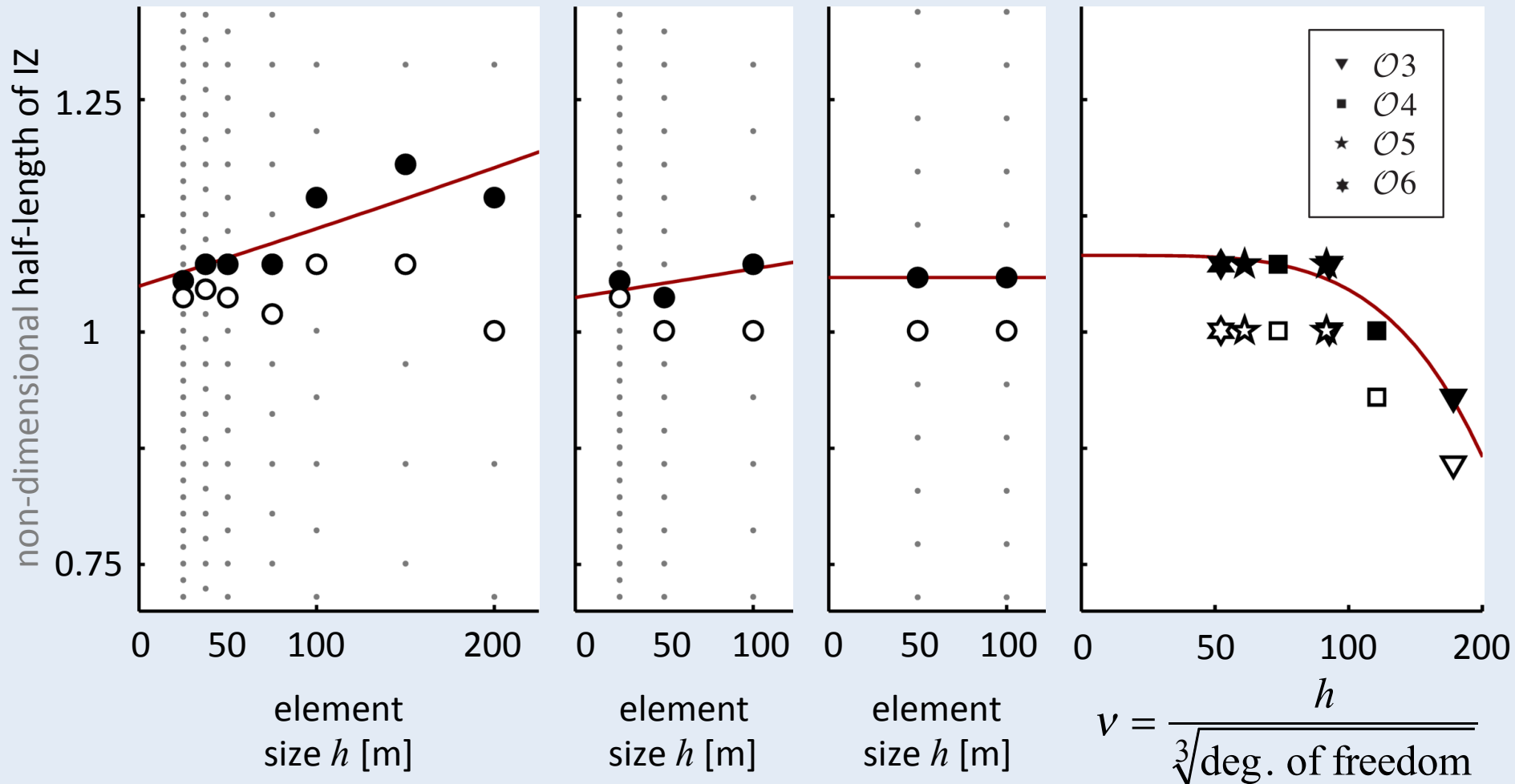
verification | high background stress, $S = 0.1$

FEM

SORD

WQLab3D

ADER-DG



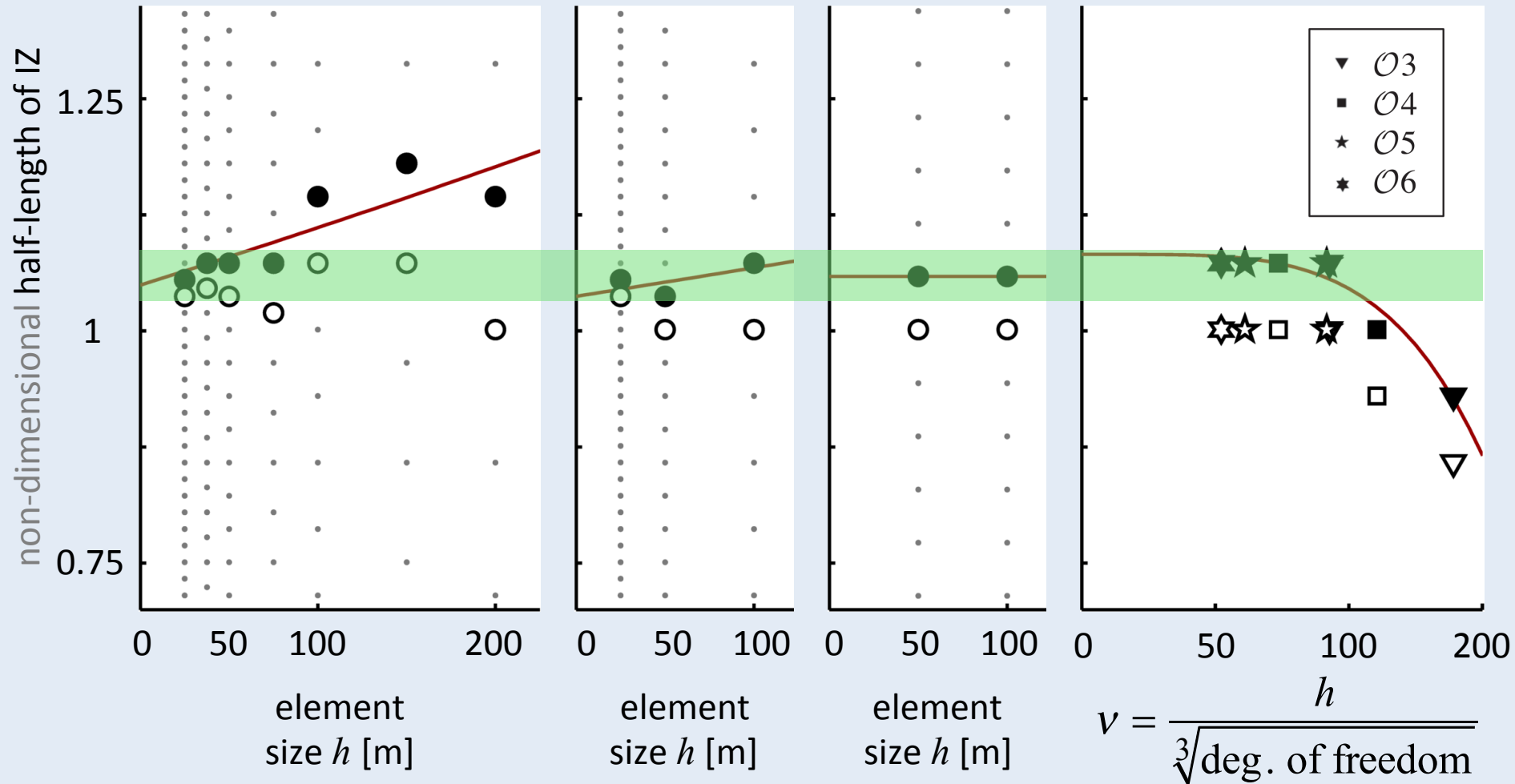
verification | high background stress, $S = 0.1$

FEM

SORD

WQLab3D

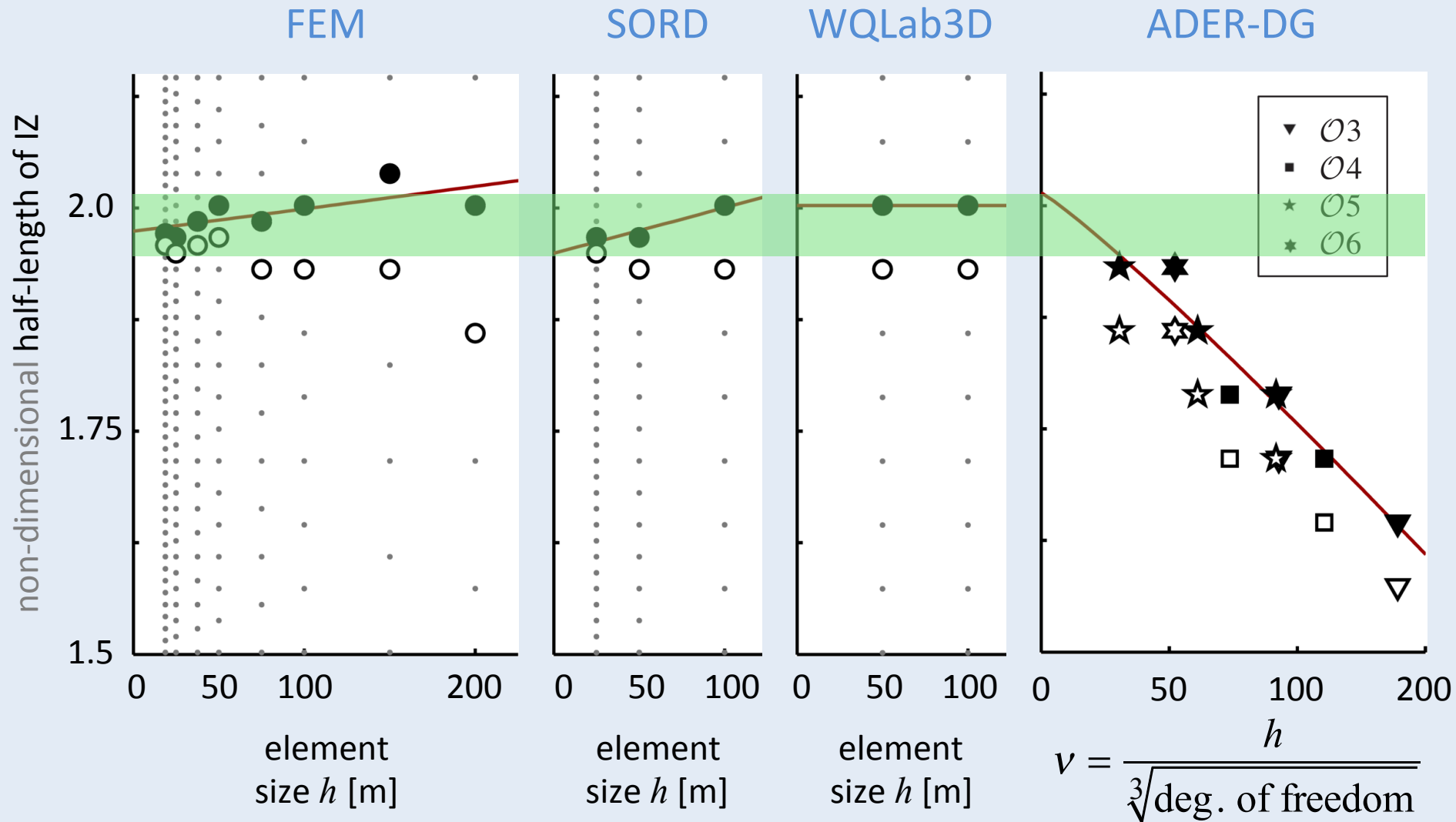
ADER-DG



the critical size of IZ converge systematically to consistent values in all 4 considered numerical methods

(within resolution of the discrete models)

verification | low background stress, $S = 2.0$



**the critical size of IZ converge systematically to consistent values
in all 4 considered numerical methods**

(within resolution of the discrete models)

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Uenishi 2009

$$L_{U3}^a \cong 0.624 C(\nu) \frac{1}{1-\nu} \frac{\mu \cdot D_c}{\tau_s - \tau_d}$$

$$L_{U3}^b \cong 0.624 C(\nu) \frac{\mu \cdot D_c}{\tau_s - \tau_d}$$

$$C(\nu) = \frac{E(k) + (1-\nu)K(k)}{2-\nu}$$

$$k = \sqrt{\nu(2-\nu)}$$

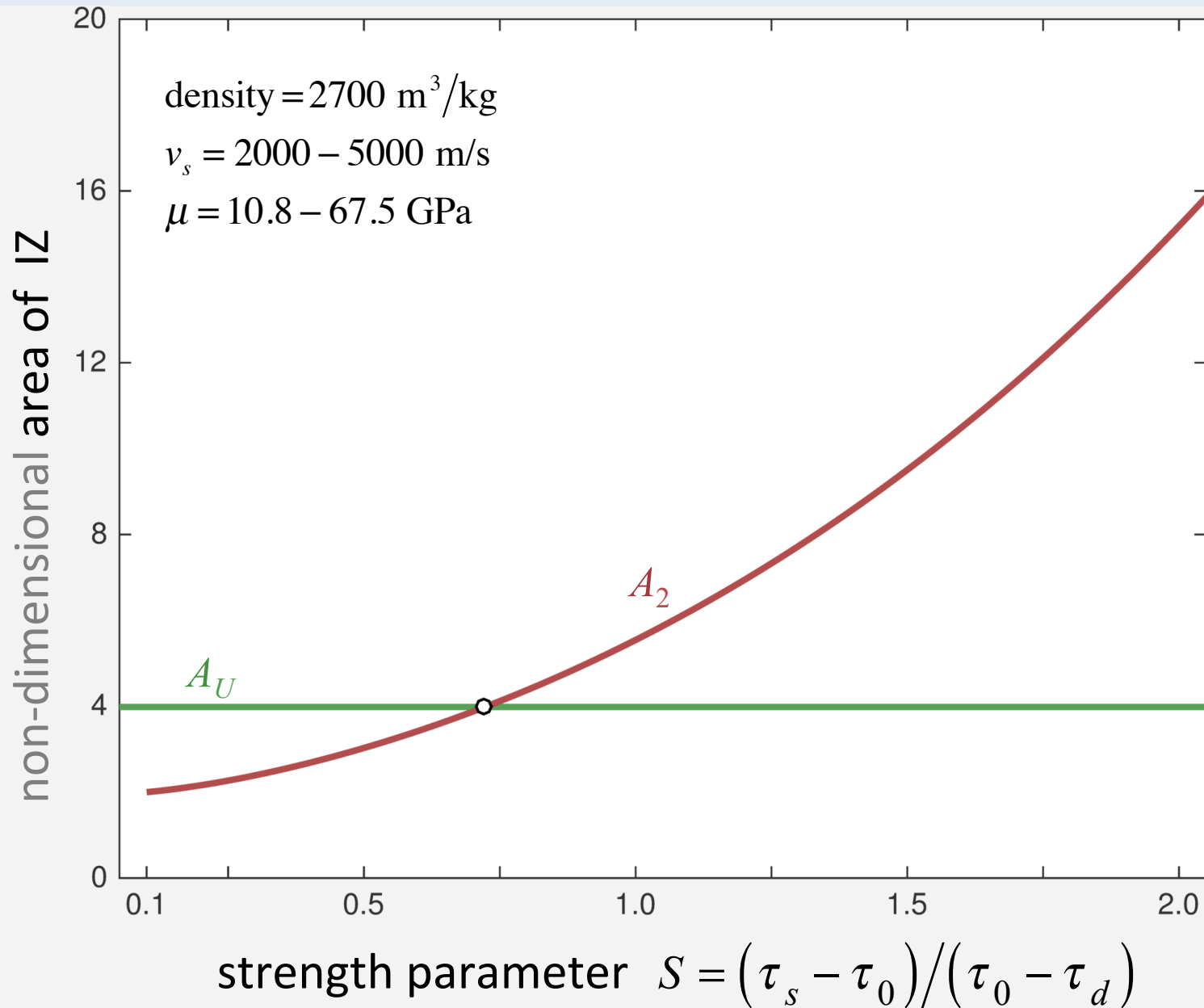
$E(k)$ and $K(k)$

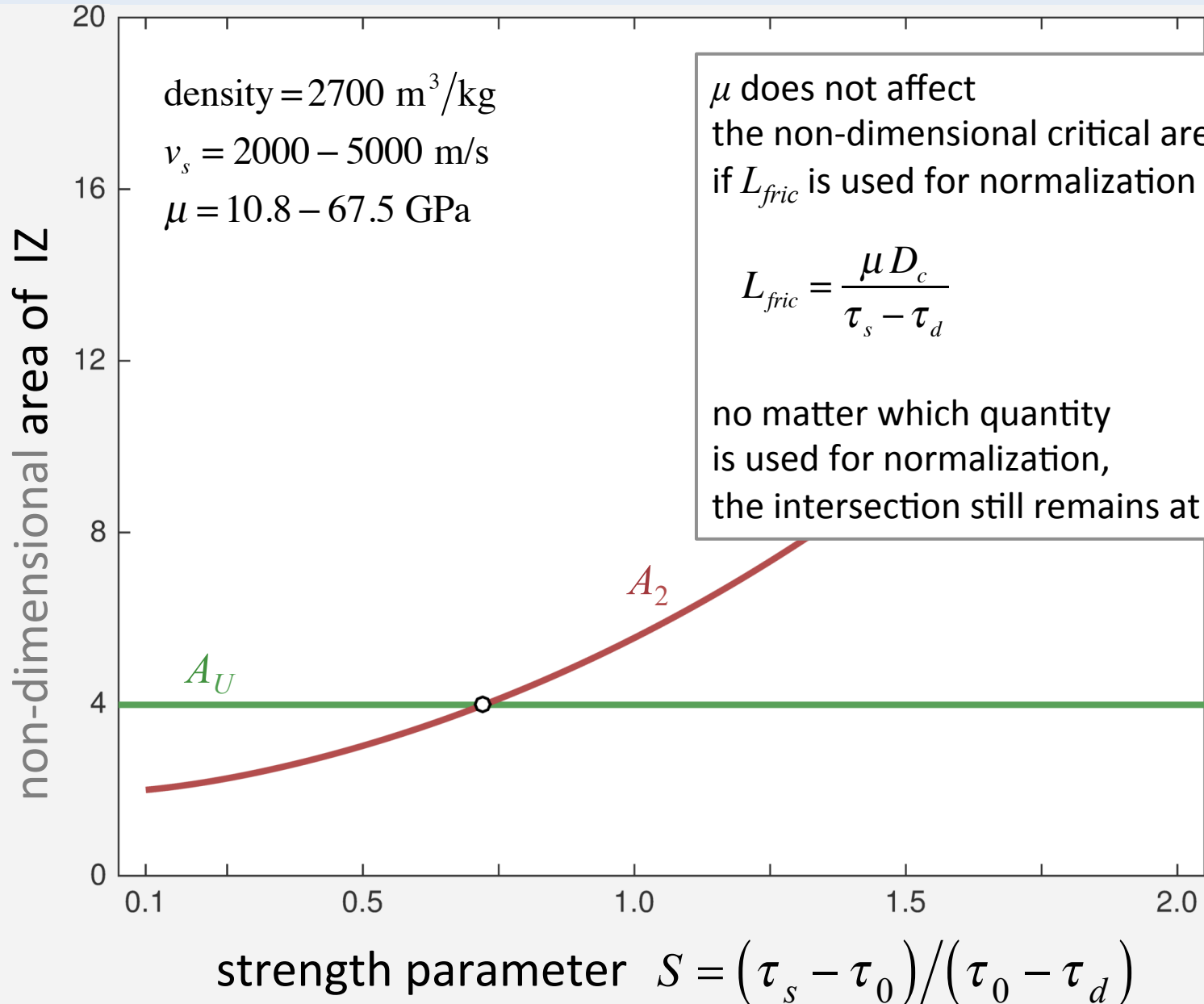
are complete elliptic integrals
of the first and second kind

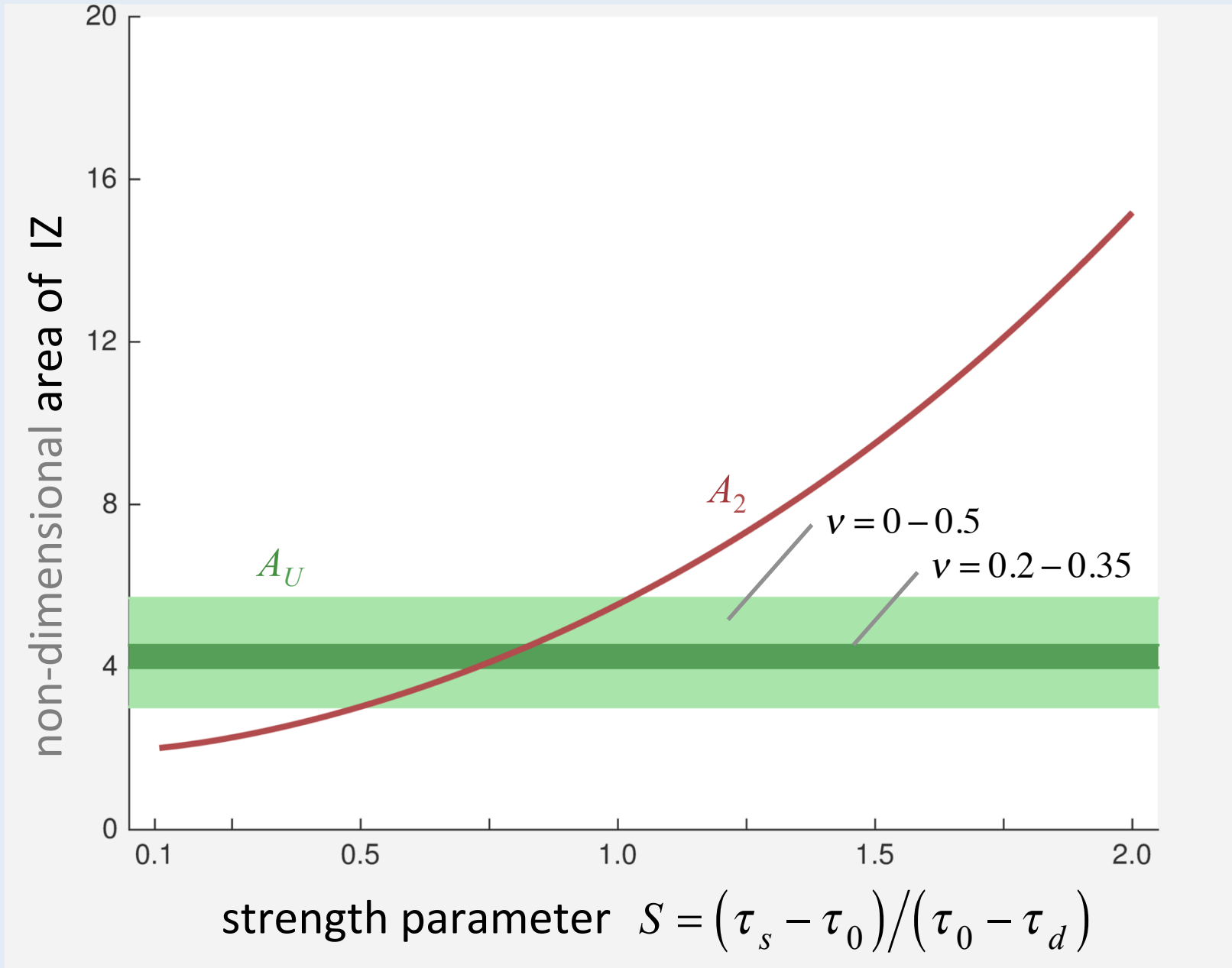
Galis et al., 2015

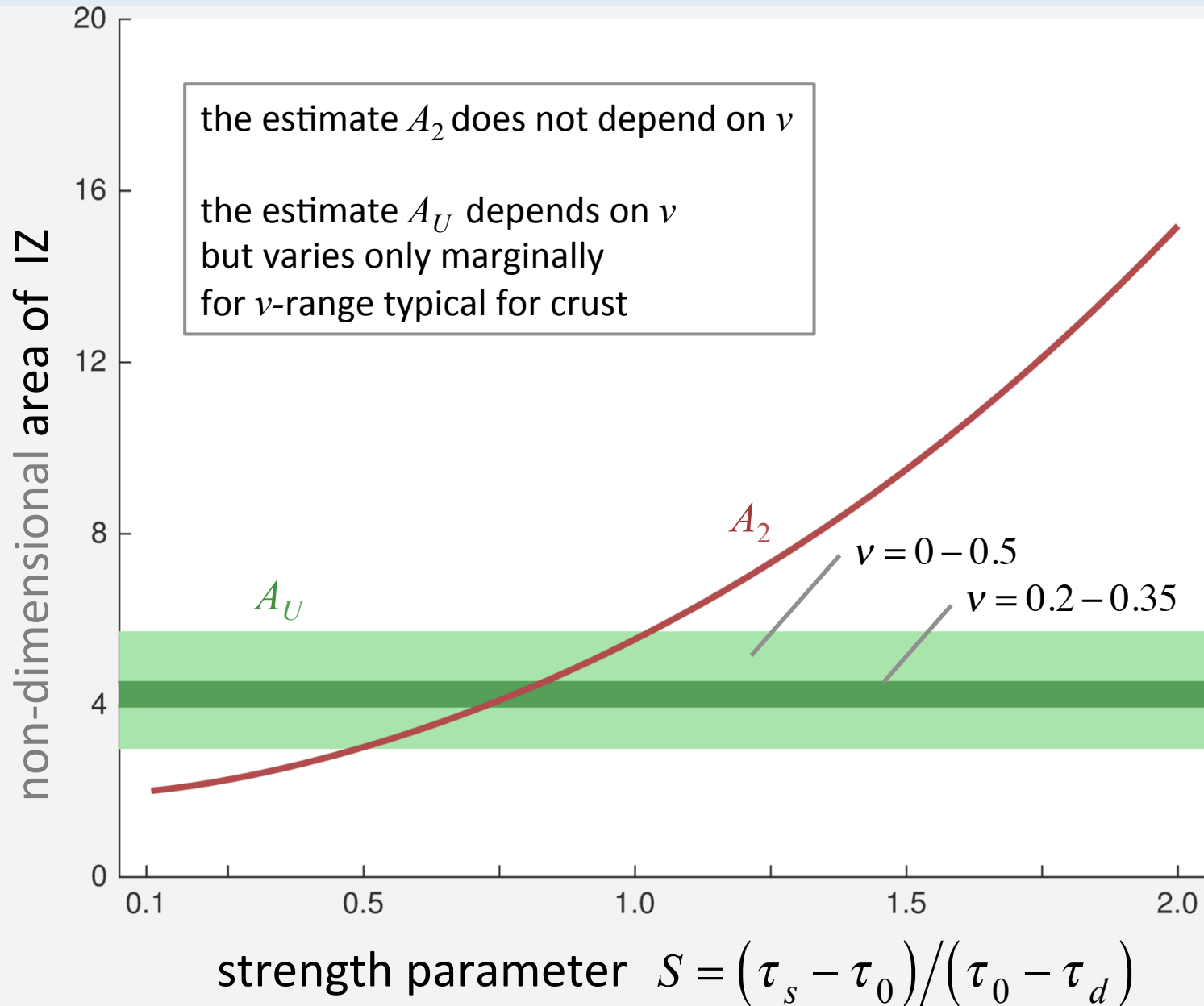
$$A_2 = \frac{\pi^3}{16} \frac{1}{f_{min}^4} \frac{(\tau_s - \tau_d)^2}{(\tau_0 - \tau_d)^4} \mu^2 D_c^2$$

$$f(x) = \sqrt{x} \left(1 + \frac{\tau_0^i - \tau_0}{\tau_0 - \tau_d} \left(1 - \sqrt{1 - 1/x^2} \right) \right)$$







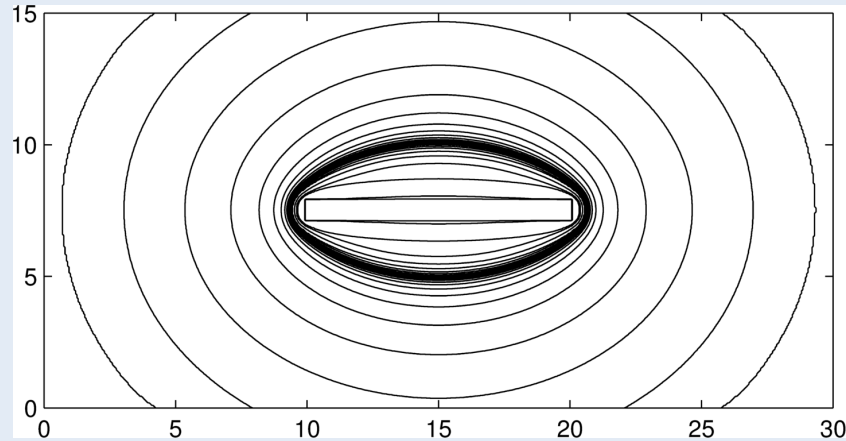


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an illustrative example
rupture initiated by

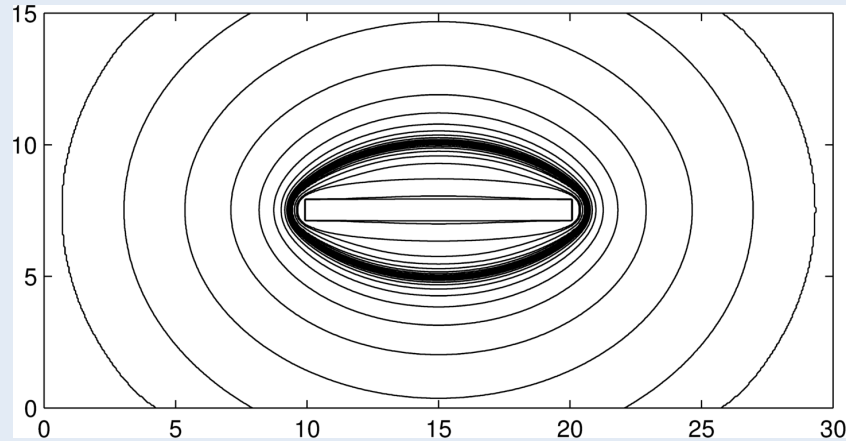
slightly over-critical parameters



- initiation with slightly over-critical parameters may take long time

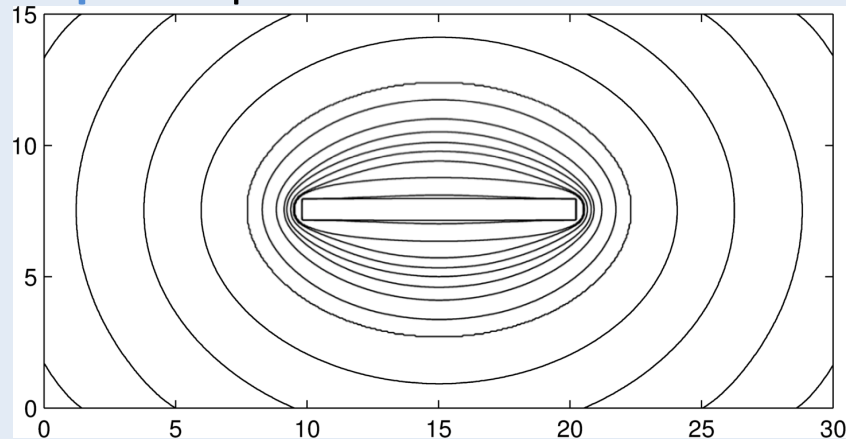
an illustrative example
rupture initiated by

slightly over-critical parameters



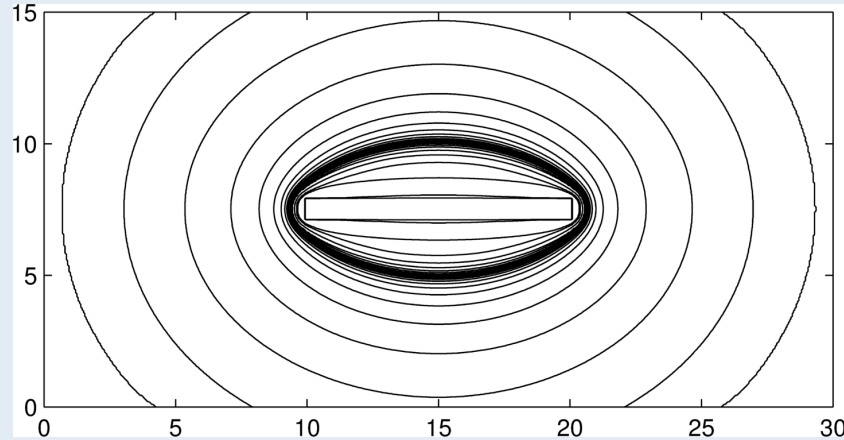
- initiation with slightly over-critical parameters may take long time

optimal parameters

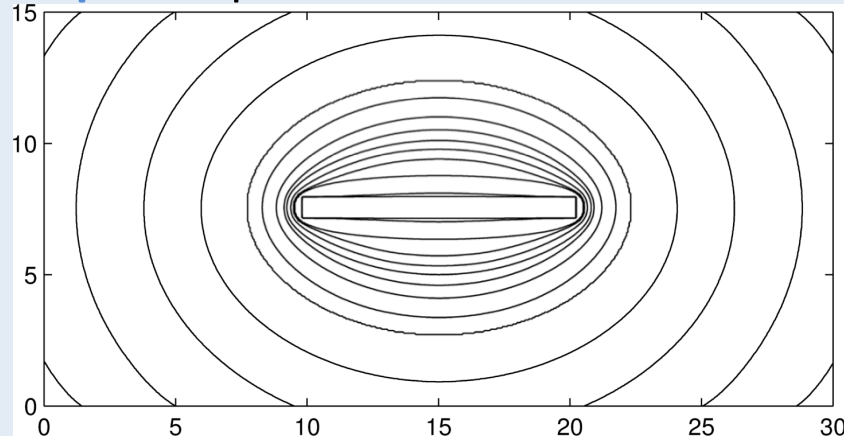


an illustrative example
rupture initiated by

slightly over-critical parameters



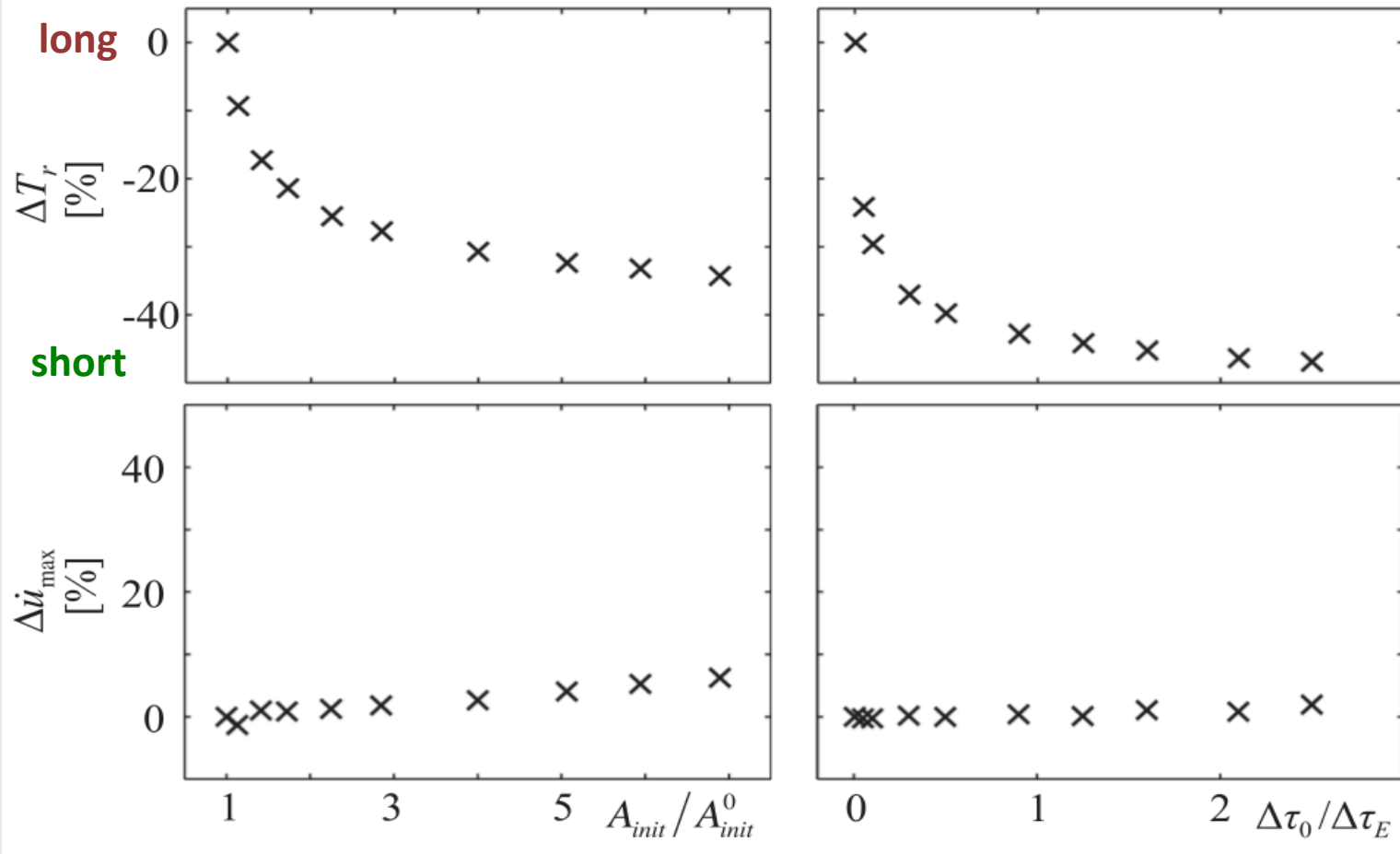
optimal parameters



- initiation with slightly over-critical parameters may take long time
- shorter duration of initiation can be achieved by **higher overstress** and/or **larger initiation area**
- if they are **too large** they can **affect resulting self-sustained dynamic rupture**
- we examine relations between the initiation area, overstress and duration of the initiation to find optimal parameters

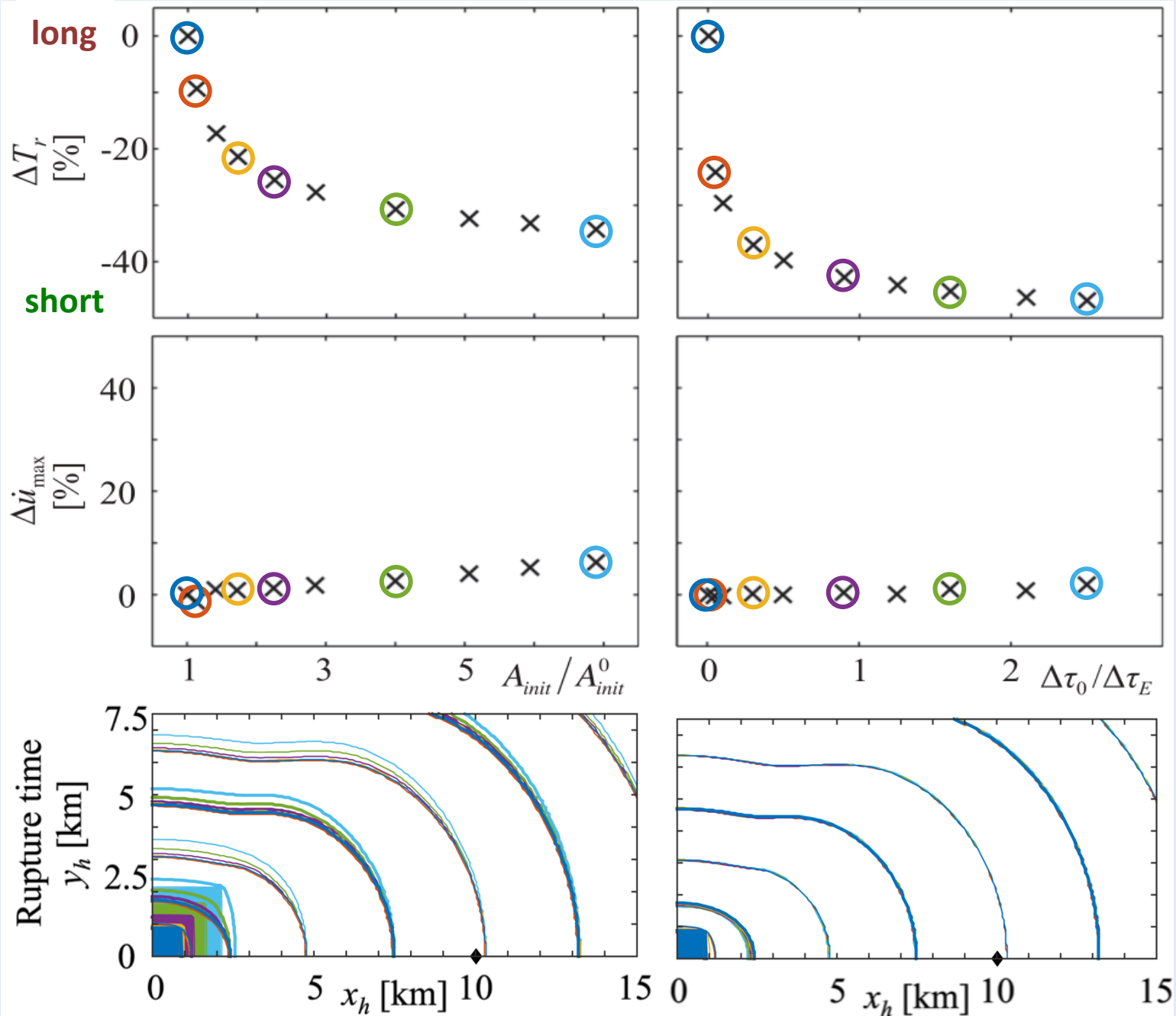
optimal parameters | high background stress, $S = 0.1$

rupture
propagation



optimal parameters | high background stress, $S = 0.1$

rupture
propagation

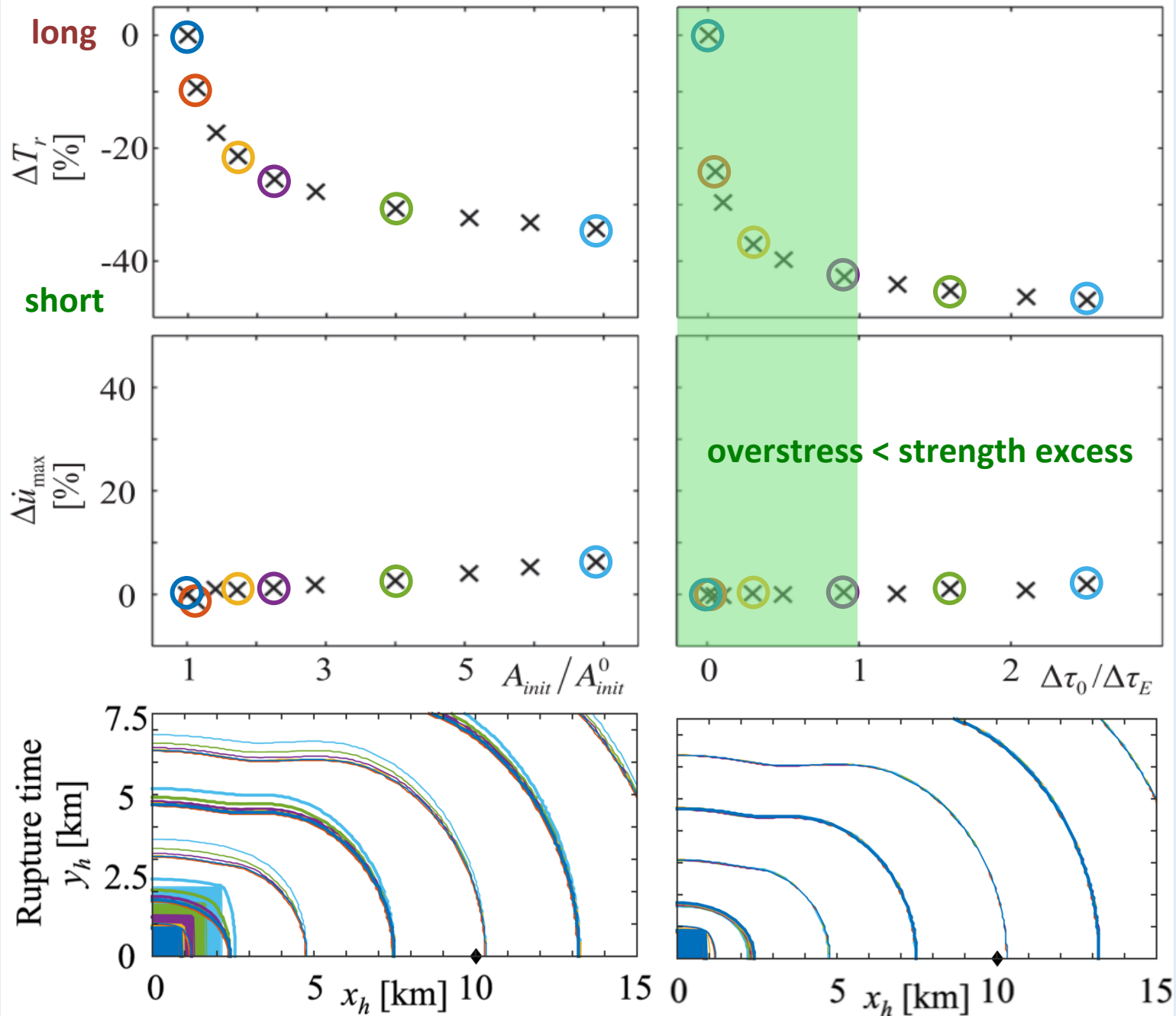


A_{init}/A_{init}^0	
1.0	2.2
1.1	3.9
1.4	6.8

$\Delta\tau_0/\Delta\tau_E$	
0.005	0.9
0.05	1.6
0.3	2.5

optimal parameters | high background stress, $S = 0.1$

rupture propagation

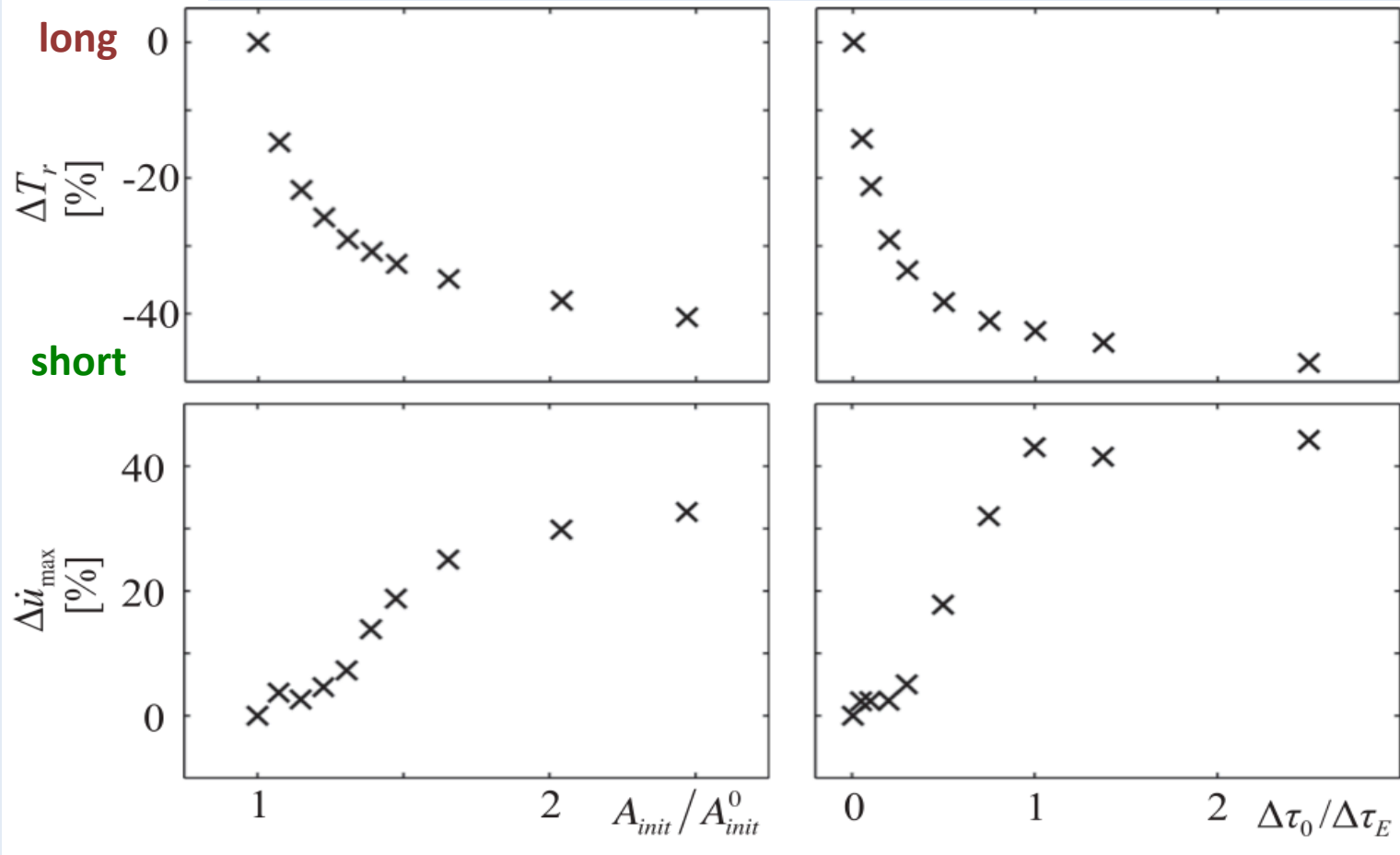


$A_{\text{init}}/A_{\text{init}}^0$	
1.0	2.2
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0.005	0.9
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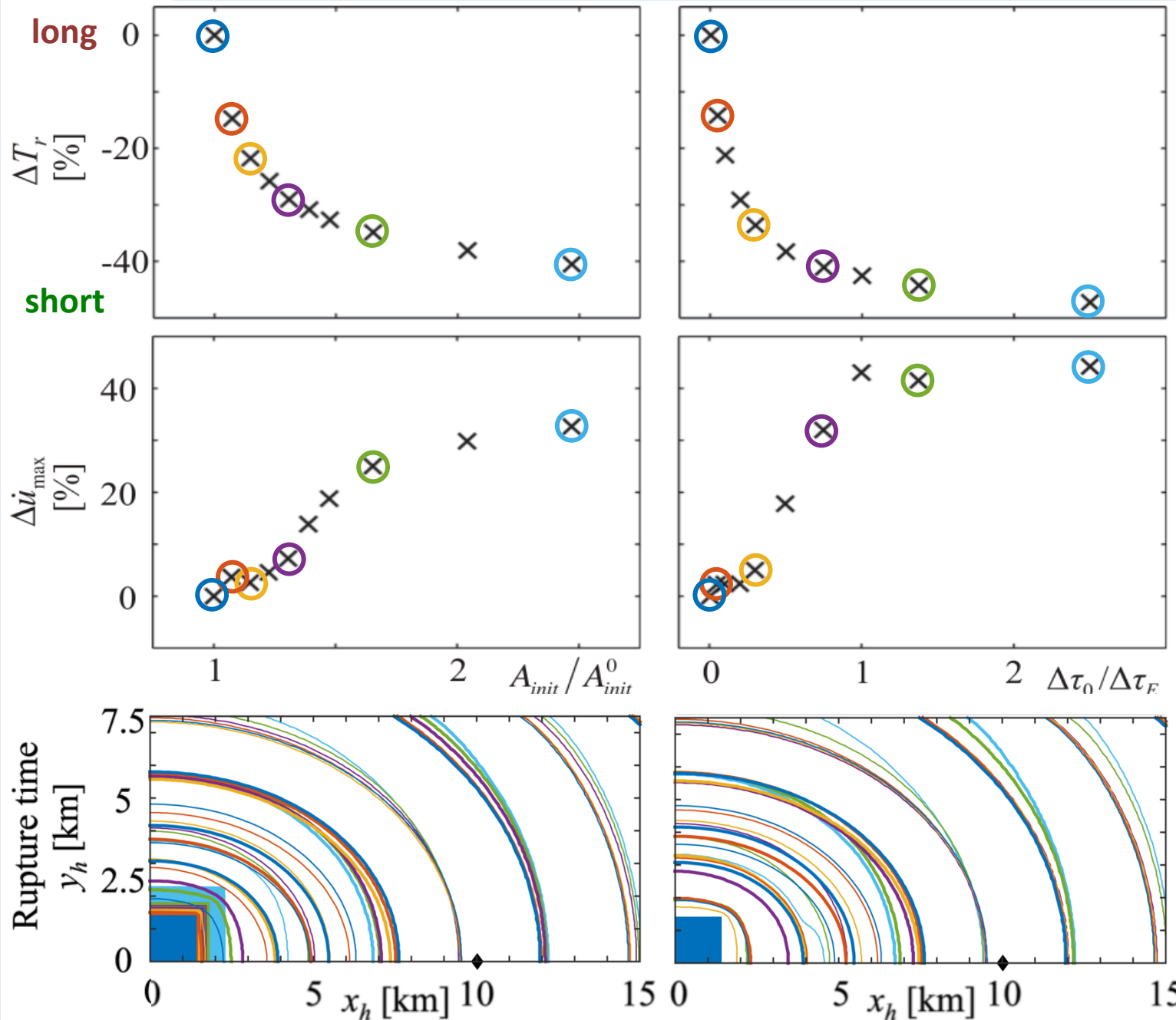
optimal parameters | low background stress, $S = 2.0$

rupture
propagation



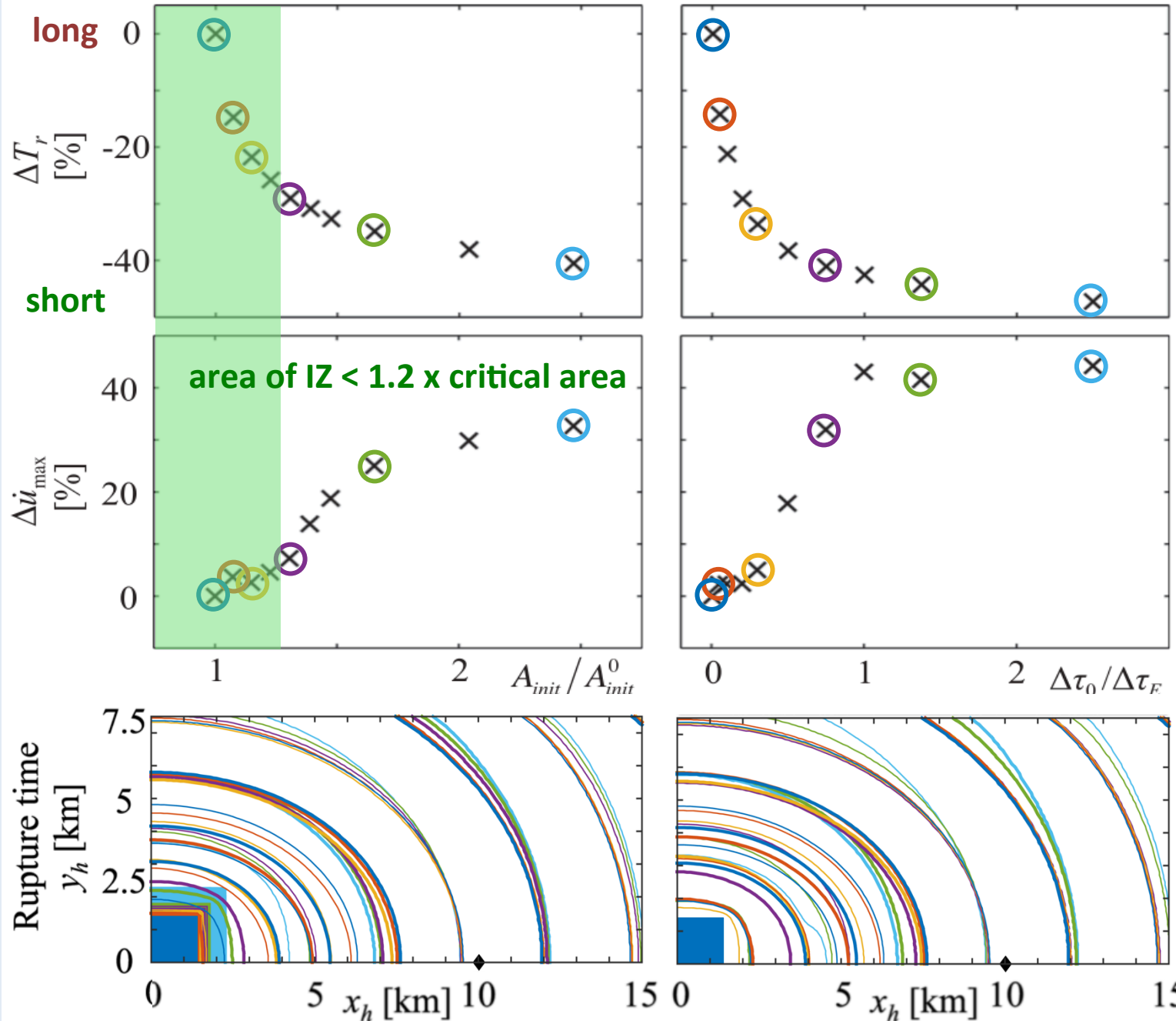
optimal parameters | low background stress, $S = 2.0$

rupture
propagation



optimal parameters | low background stress, $S = 2.0$

rupture propagation



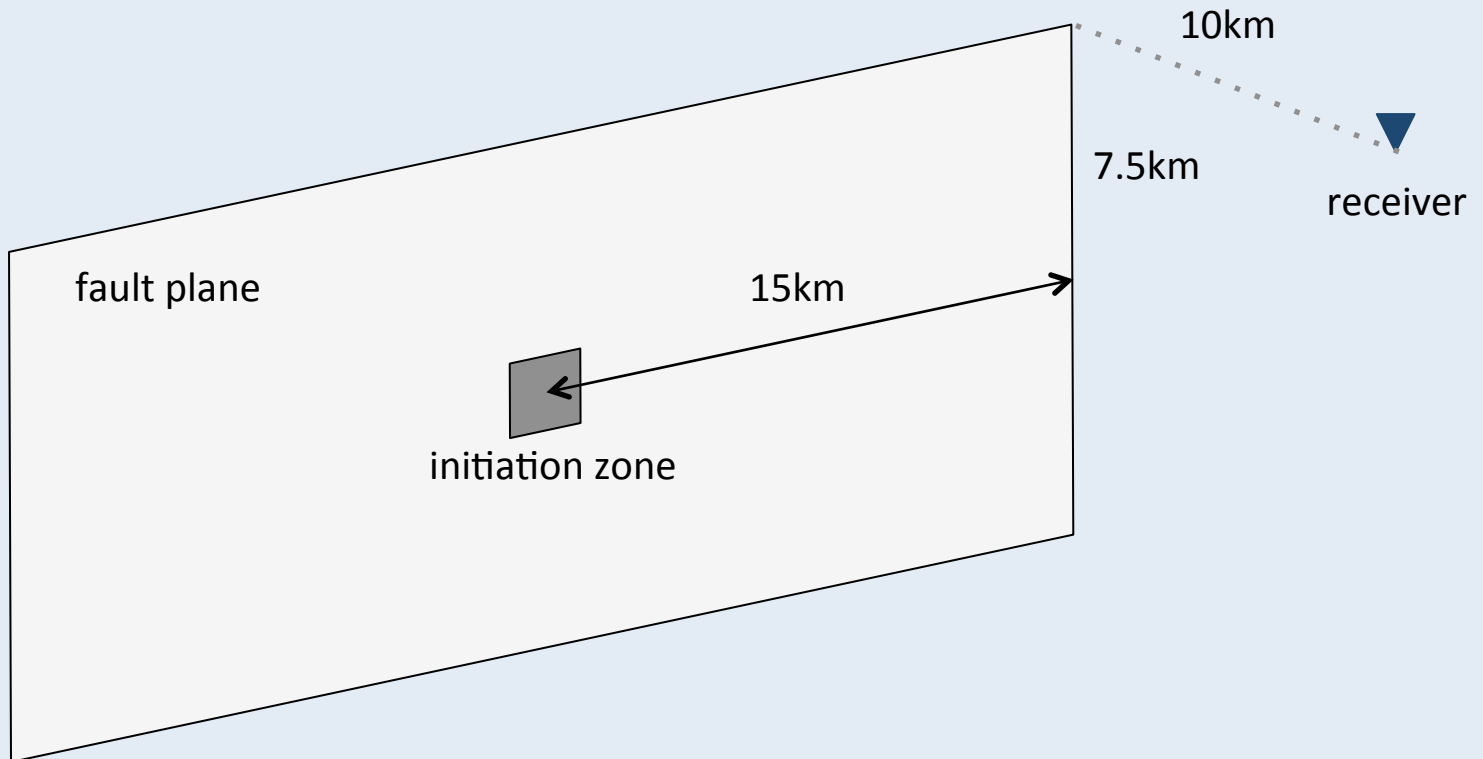
$A_{\text{init}} / A_{\text{init}}^0$	
1.0	1.4
1.1	1.7
1.2	2.5

$\Delta \tau_0 / \Delta \tau_E$	
0.005	0.9
0.05	1.6
0.3	2.5

Galis et al., 2015

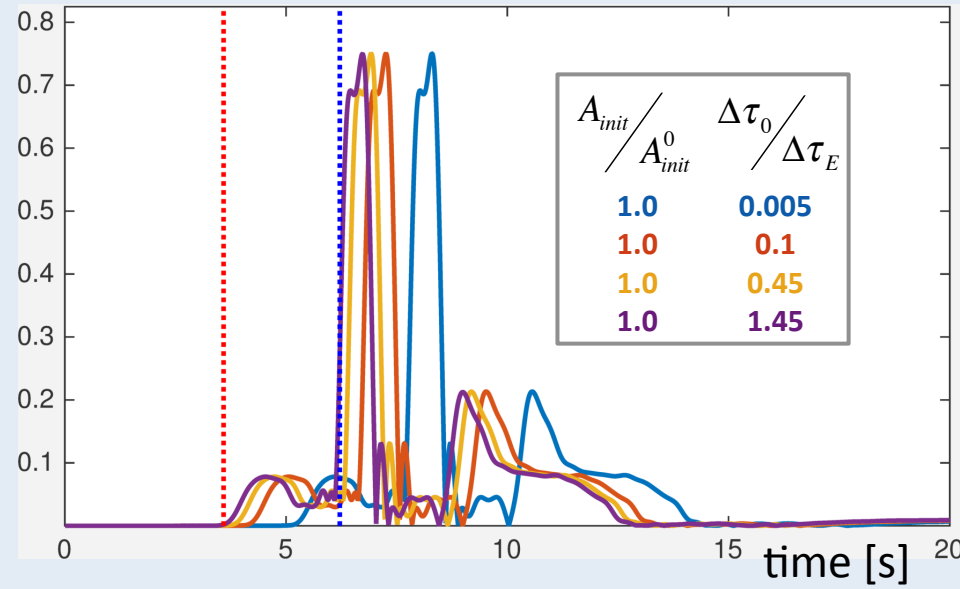
analyzed effects of initiation on rupture propagation

we now extend the analysis to effects on ground motion

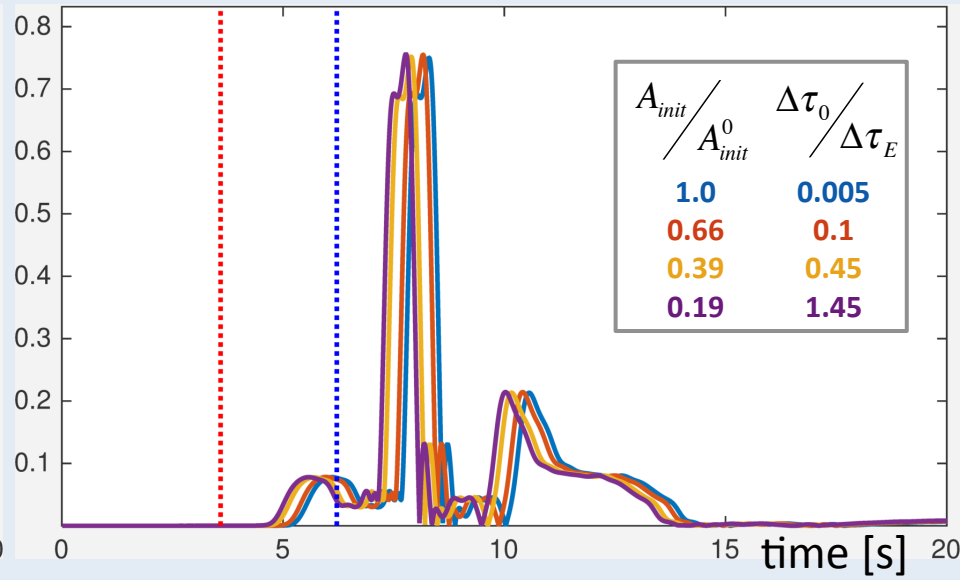


comparison of magnitude of particle velocity

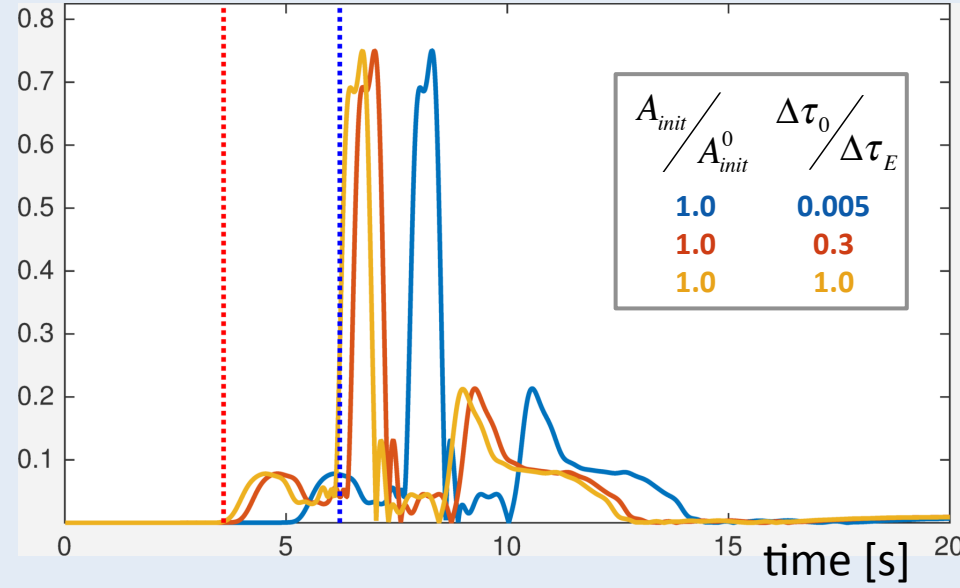
super-critical initiation



slightly overcritical initiation



optimal initiation

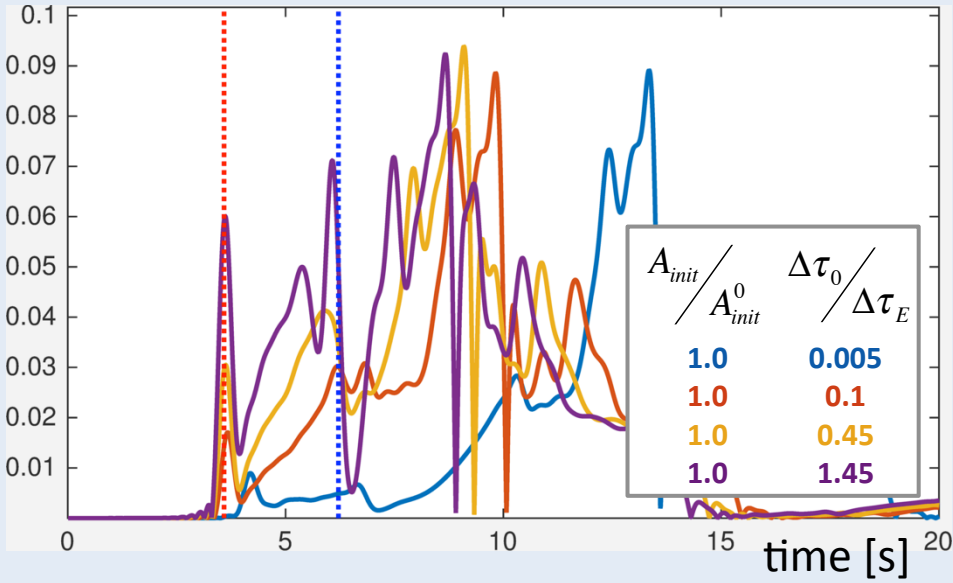


no observable
hypo-central P- or S- waves

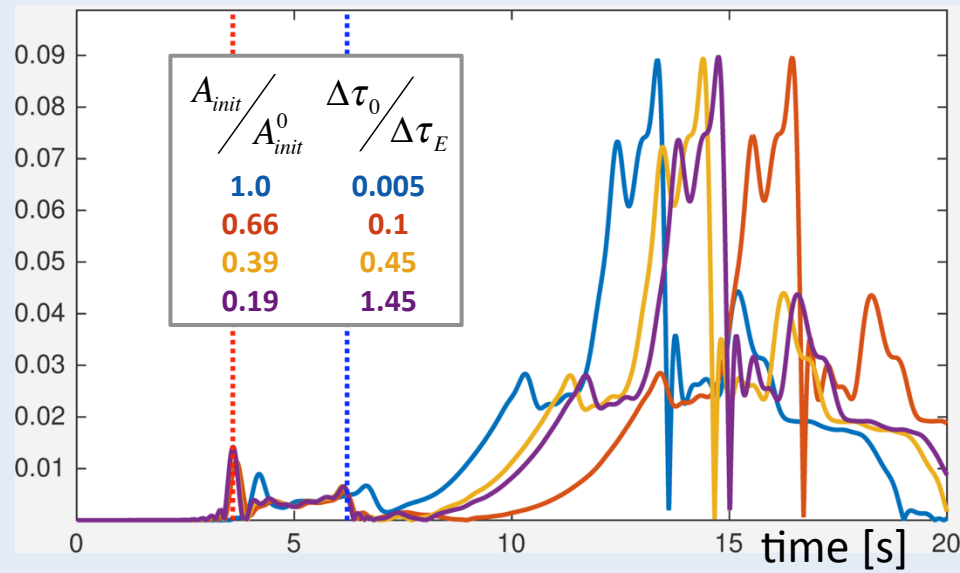
optimal initiation:
overstress < strength excess

comparison of magnitude of particle velocity

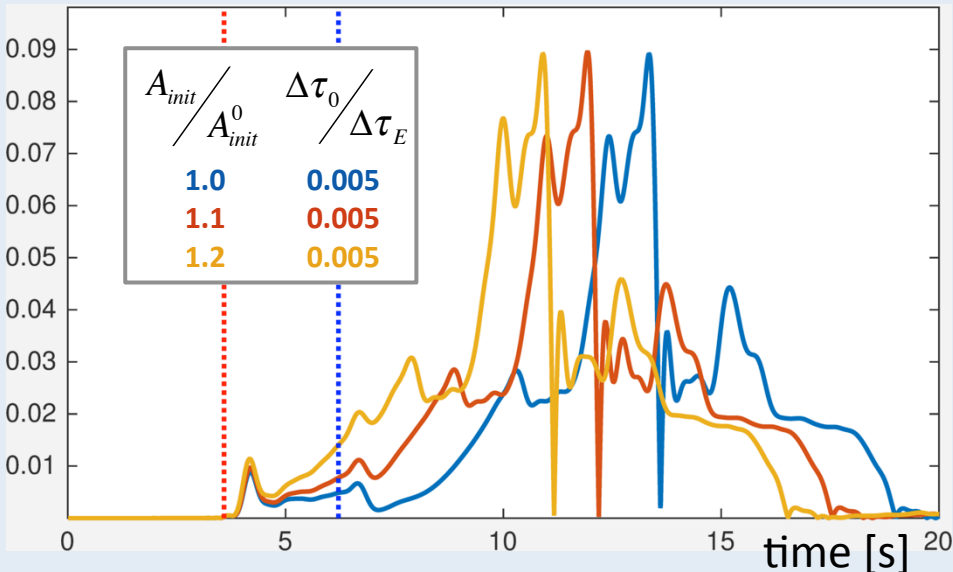
super-critical initiation



slightly overcritical initiation



optimal initiation



super-critical initiation:

strong hypo-central P- or S- waves

slightly overcritical and optimal initiation:

marginal variations in
hypo-central P- or S- waves

optimal initiation:

area < 1.2 x critical area

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summary

- for a fixed overstress and aspect ratio close to 1
the initiation is controlled by the area of the initiation zone
however, if one side of IZ should be shorter
than the corresponding critical half-length
initiation is controlled by half-length

- **the critical area** can be estimated by

$$A_{crit} = \max(A_U, A_2)$$

A_U : estimate by Uenishi, 2009

A_2 : estimate by Galis et al., 2015

- **efficient initiation with minimized side effects**
on rupture propagation and ground motion
can be achieved

high background stress (low S)

low background stress (high S)

overstress < strength excess

area of IZ < 1.2 x critical area

An aerial photograph of a dense forest with a winding road. The image is in a monochromatic blue color scheme. The road curves through the trees, and the overall texture is highly detailed due to the canopy. The text 'Thank you' is centered over the middle of the image.

Thank you

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